Table of Contents: Notes: this page BQ24745 Battery charger: from page 2 3 Li-ion cell with 4.2V target per cell or 12.6V overall application: Up to 10 A with airflow: pages 2-4 (efficiency & losses, thermal image, major waveform) Up to 8 A without airflow: pages 5-7 (eff. & losses, thermal image, major waveform)

1 Li-ion cell with 4.2V target and 5 A max application: page 8

"AC drive" turn on with 24Vin: page 9

TPS40170 & 2xCSD18504 converter for 5V at 4A: pages 10-12 (main waveform, start up, output ripple, Bode plot, losses & efficiency)

TPS54335 integrated converter for 12V or 5V to 2 A: pages 13-16 (efficiency & losses, main waveform, ripple out, Bode plots)

Notes:

To allow 10 A out of the BQ24745 converter instead of 8 A, the Battery current sense (R17 in schematic) was changed from 10 mOhms to 8 mOhms. Hence, battery current limit settings from the BQ24745 GUI need to be multiplied by 1.25. Input current sense R1 is at standard 10 mOhms. Hence, GUI input current settings are correct.

Q7 must be mounted with metal tab away from J5. Q7 silkscreen on rev A PCB is not clear enough.

Limitations: Currents above 8A charging off 24Vin will need airflow as Q5 rises 50 deg. C above ambient at 8A current and no fan.

For lower charging voltage applications, such as single Li-ion cells:

"Fixed" current limit of about 3 A for Vout below 4 V in the BQ24745 becomes about 3.75 A. This protection limit was put in for multi-cell applications that the BQ24745 targeted; but does limit charging current during most of the recharge of single Li-ion cell applications where battery voltage is below 4V. Increasing current limit in such applications beyond this 3.75A will have limited effect in speeding up overall charging, as most of current limited charging occurs with battery less than 4V. For the testing shown here 5A was targeted to show transition out of the "3.75A mode".

When Vout less than 4V charging limited to 3A/(0.8) or 3.75A nominal and 3.70A on model t1. When battery V rose slightly above 4.0V, charging current increased to full 4.1A / (0.8) or 5A.

Battery discharge FET Q7 conduction verified on all 3 models with load resistance connected to J5 adjusted to target about 5 A:

Battery discharge on model t1: 5.23A at 131mV across Q7. Battery discharge on model t2: 5A at 120mV across Q7. Battery discharge on model t3: 5.1A at 120mV across Q7. PMP-9668 Universal Battery Charger off 24Vin Test Report (BQ24745) Texas Instruments

BQ24745 converter with ~200 LFM airflow:

Efficiency and Losses: model t2: 24.0 Vin, Vout set at 12.6V

For efficiency & loss calculations I have subtracted out from the measured Iin values shown here, the 26mA drawn by 5V4A converter off the 24V

forced air about 200 LFM *italicized with* R9 = 24.9, else R9 = 15. R9 is gate drive resistor.

| Vin | Iin A | Vout | Iout | % Effi | Losses in W | comments |
|--------|--------|---------|--------|--------|-------------|-----------------|
| Volts | | Volts | А | ciency | | |
| 24.09 | 0.002 | all | off | | | 5V inhibited |
| 24.09 | 0.028 | only | 5V on | | | |
| 24.09 | 0.030 | < lV | 0 | | | I chrg set 0 |
| 24.09 | 0.0455 | 4.215 | 0 | | | 4.208Vset |
| 24.09 | 0.0605 | 12.62 | 0 | | | 12.608 set |
| 24.025 | 5.420 | 12.227 | 9.968 | 94.0 | 7.712 | |
| 24.07 | 5.455 | 12.347 | 9.968 | 94.2 | 7.601 | |
| 24.07 | 5.433 | 12.296 | 9.965 | | | Ir469 69 max on |
| | | | | 94.1 | 7.617 | Q5 |
| 24.08 | 5.437 | 12.503 | 9.814 | 94.2 | 7.592 | |
| 24.09 | 5.305 | 12.615 | 9.516 | 94.4 | 7.127 | |
| 24.06 | 5.023 | 12.618 | 9.006 | 94.5 | 6.590 | |
| 24.09 | 4.730 | 12.617 | 8.501 | 94.7 | 6.062 | |
| 24.07 | 4.457 | 12.618 | 8.009 | 94.8 | 5.597 | |
| 24.06 | 4.862 | 11.052 | 9.870 | 93.8 | 7.271 | |
| 24.03 | 4.374 | 10.008 | 9.750 | 93.4 | 6.904 | |
| 24.07 | 3.900 | 9.021 | 9.616 | 93.0 | 6.501 | |
| 24.07 | 3.902 | 12.617 | 7.019 | 94.9 | 4.737 | |
| 24.05 | 3.341 | 12.618 | 6.009 | 95.1 | 3.904 | |
| 24.04 | 2.7905 | 12.617 | 5.006 | 95.0 | 3.298 | |
| 24.095 | 2.234 | 12.618 | 4.002 | 94.9 | 2.705 | |
| 24.045 | 1.6957 | 12.618 | 3.003 | 94.4 | 2.256 | |
| 24.035 | 1.1520 | 12.6175 | 2.0035 | 93.4 | 1.784 | |
| 24.085 | 0.6060 | 12.620 | 1.0013 | 90.5 | 1.333 | |
| 24.08 | 0.3295 | 12.622 | 0.5013 | 86.6 | 0.981 | |
| 24.11 | 0.0605 | 12.622 | 0 | 0.0 | 0.832 | |
| 24.11 | 0.0277 | off | | | | |
| | | | | | | |

Model t2: (models t1& t3 went for software integration) 305kHz actual vs. 300kHz target at 10A out

PMP-9668 Universal Battery Charger off 24Vin Test Report (BQ24745) Texas Instruments

Thermal Image at near max current with airflow:

PMP9668A model t2 charger 305kHz 24.07Vin 12.296Vout 9.965Aout 7.617W diss in charger ~200 LFM airflow 21-23 deg. C ambient Q5 at 69, Q6 at 52, inductor top 55, snubber R at 45, snubber C at 50, R1 at 60, R17 at 57





Major waveform: 24Vin near 10A out R9 (gate drive resistor) at 24.9 ohms: $^{7-May-14}_{17:10:39}$

Same, but R9 (gate drive resistor) at 15 ohms:



About 0.6V below 30V max of BQ24745 and well below 40V rating of CSD18504

BQ24745 converter with no forced airflow: 8 A max here

Efficiency and Losses: model t2: 24.0 Vin, Vout set at 12.6V

For efficiency & loss calculations I have subtracted out from the measured Iin values shown here, the 26mA drawn by 5V4A converter off the 24V

| Vin | Iin A | Vout | Iout | % Effi | Losses in W | comments |
|--------|--------|--------|--------|--------|-------------|--------------|
| Volts | | Volts | А | ciency | | |
| 24.06 | 4.3155 | 12.453 | 7.847 | | | IR470 20 min |
| | | | | 94.7 | 5.487 | 72max |
| 24.07 | 4.200 | 12.001 | 7.916 | 94.6 | 5.468 | |
| 24.07 | 3.871 | 11.012 | 7.916 | 94.2 | 5.378 | |
| 24.10 | 3.532 | 10.010 | 7.916 | 93.8 | 5.255 | |
| 24.02 | 3.100 | 9.003 | 7.669 | 93.5 | 4.793 | |
| 24.05 | 4.346 | 12.439 | 7.911 | | | Vds on Q6 |
| | | | | 94.7 | 5.491 | 28.6Vmax |
| 24.05 | 4.284 | 12.604 | 7.702 | 94.8 | 5.329 | |
| 24.07 | 4.171 | 12.619 | 7.4985 | 94.8 | 5.147 | |
| 24.06 | 3.898 | 12.621 | 7.007 | 94.9 | 4.725 | |
| 24.04 | 3.343 | 12.621 | 6.007 | 95.1 | 3.926 | |
| 24.09 | 2.784 | 12.621 | 5.004 | 95.1 | 3.285 | |
| 24.01 | 2.245 | 12.621 | 4.007 | 94.9 | 2.706 | |
| 24.065 | 1.6952 | 12.621 | 3.002 | 94.3 | 2.281 | |
| 24.005 | 1.1530 | 12.621 | 2.0015 | 93.4 | 1.793 | |
| 24.05 | 0.6071 | 12.622 | 1.0014 | 90.4 | 1.336 | |
| 24.08 | 0.3290 | 12.623 | 0.4995 | 86.4 | 0.991 | |
| 24.10 | 0.0604 | 12.623 | 0 | 0.0 | 0.829 | |
| | | | | | | |
| | | | | | | |

No forced air R9 = 15 max I will target 8A or 6400mA divided by 0.8

Model t2: (model t1 went for software integration) 305kHz actual vs. 300kHz target at 8A out

PMP-9668 Universal Battery Charger off 24Vin Test Report (BQ24745) Texas Instruments

PMP9668A model t2 charger 305kHz 24.06Vin 12.453Vout 7.847Aout 5.487W dissipation in charger convection only 21-23 deg. C ambient Q5 at 72, Q6 at 59, inductor top 70, snubber R at 53, snubber C at 57.6, R17 at 59



q



Major waveform at 24vin and near 8A out convection cooled: $7-Ma_{11}-14$

Efficiency and Losses: model t2: 24.0 Vin, Vout set at 4.208V For efficiency & loss calculations I have subtracted out from the measured Iin values shown here, the 26mA drawn by 5V4A converter off the 24V

| Vin | Iin A | Vout | Iout | % Effi | Losses in W | comments |
|--------|----------|-------|--------|--------|-------------|------------------|
| Volts | | Volts | А | ciency | | |
| 24.09 | 0.044 | 4.215 | 0 | 0.0 | 0.434 | |
| 24.06 | 0.997 | 4.159 | 5.035 | | | Max lin 52 degC |
| | | | | 89.6 | 2.422 | hotspot |
| 24.06 | 0.990 | 4.100 | 5.065 | 89.5 | 2.427 | |
| 24.06 | 0.969 | 3.997 | 5.074 | 89.4 | 2.408 | |
| 24.06 | 0.935 | 3.838 | 5.076 | | | Falling drops as |
| | | | | 00.4 | 0.000 | Vout drops |
| | 0.10-7-7 | 0.550 | 0.444 | 89.1 | 2.389 | below 3.83V |
| 24.01 | 0.6375 | 3.552 | 3.646 | 88.2 | 1.732 | 3A/0.8 mode |
| 24.02 | 0.552 | 3.006 | 3.647 | 86.8 | 1.672 | 3A/0.8 mode |
| 23.99 | 0.942 | 3.861 | 5.079 | | | Just b4 3A/0.8 |
| | | | | 89.2 | 2.365 | mode |
| 24.01 | 0.707 | 3.998 | 3.643 | 89.1 | 1.786 | 3A/0.8 mode |
| 24.03 | 0.487 | 2.592 | 3.648 | 85.4 | 1.622 | 3A/0.8 mode |
| | | | | | | |
| 24.025 | 0.9855 | 4.201 | 4.928 | 89.8 | 2.349 | |
| 24.03 | 0.9063 | 4.213 | 4.507 | 89.8 | 2.166 | |
| 24.04 | 0.8099 | 4.213 | 4.007 | 89.6 | 1.963 | |
| 24.06 | 0.6186 | 4.214 | 3.006 | 88.8 | 1.591 | |
| 24.075 | 0.4313 | 4.214 | 2.000 | 86.4 | 1.330 | |
| 24.09 | 0.2407 | 4.215 | 1.002 | 81.7 | 0.949 | |
| 24.06 | 0.1558 | 4.215 | 0.5000 | 67.5 | 1.015 | |
| 24.07 | 0.0433 | 4.214 | 0 | 0.0 | 0.416 | |
| | | | | | | |
| 24.05 | 0.238 | 1.397 | 2.042 | 56.0 | 2.246 | |

No forced air R9 = 15 max I will target 5A or 4096mA divided by 0.8

Model t2: (model t1 went for software integration) 305kHz actual vs. 300kHz target at 5A out

Enters 3A/0.8 mode on Vout falling below 3.84V and exits it at 4.03V rising. Short circuit current for Vout less than 2.49V falling or 2.7V rising is in 1.3 to 2.1A range.



ACDRV turn on and rise of output of Q1 –Q2 blocking transistors: 24Vin: 2-May-14 16:22:16



5V4A testing: R107 updated from zero to 5.1 to reduce peak Vds stress on Q102 from nearly 39V to under 35V: Switching frequency 376kHz





5V4A efficiency & losses: 24Vin, 376kHz switching on model t2 after R107 changed to 5.1 ohms; 2mA of input current already subtracted out as due to other circuits

| No | fans; | full | load | hotspot | just und | ler 50 | degrees | C per | Thermal | camera |
|----|-------|------|------|---------|----------|--------|---------|-------|---------|--------|
|----|-------|------|------|---------|----------|--------|---------|-------|---------|--------|

| Vin | Iin A | Vout | Iout | % Effi | Losses in W | comments |
|-------|--------|-------|-------|--------|-------------|----------|
| Volts | | Volts | A | ciency | | |
| 24.08 | 0.9327 | 4.928 | 4.084 | 89.6 | 2.333 | |
| 24.05 | 0.6832 | 4.924 | 3.000 | 89.9 | 1.659 | |
| 24.07 | 0.4587 | 4.918 | 2.001 | 89.1 | 1.200 | |
| 24.09 | 0.2413 | 4.920 | 1.001 | 84.7 | 0.888 | |
| 24.10 | 0.1342 | 4.957 | 0.500 | 76.6 | 0.756 | |
| 24.11 | 0.0252 | 4.960 | 0 | N/A | 0.608 | |
| | | | | | | |

Converter is fixed frequency without light load reduced frequency / conduction.

Q

5V or 12V at 2A aux output off 24Vin:

efficiency & losses: 24Vin, 583kHz switching on model t2 with other converters inhibited; 2mA of input current already subtracted out as due to other circuits (mostly BQ24745 and related circuits)

No fans; full load hotspot on TPS54335DDA 45 degrees C per Thermal camera, inductor top about 30 degrees C pointing to low core losses in Vishay part

Converter is with light load reduced frequency / conduction.

| Vin | Iin A | Vout | Iout | % Effi | Losses in W | comments |
|--------|--------|--------|--------|--------|-------------|----------|
| Volts | | Volts | А | ciency | | |
| 24.06 | 1.0598 | 11.884 | 2.0145 | 93.9 | 1.558 | |
| 24.09 | 0.7850 | 11.892 | 1.501 | 94.4 | 1.061 | |
| 24.03 | 0.5238 | 11.900 | 1.001 | 94.6 | 0.675 | |
| 24.055 | 0.2635 | 11.908 | 0.5001 | 94.0 | 0.383 | |
| 24.08 | 0.0004 | 11.918 | 0 | N/A | 0.010 | |
| | | | | | | |
| 24.03 | 0.4747 | 4.975 | 2.013 | 87.8 | 1.392 | |
| 24.05 | 0.3495 | 4.978 | 1.500 | 88.8 | 0.938 | |
| 24.06 | 2.330 | 4.982 | 1.000 | 88.9 | 0.624 | |
| 24.07 | 0.1169 | 4.985 | 0.5026 | 89.0 | 0.308 | |
| 24.08 | 0.0003 | 4.991 | 0 | N/A | 0.007 | |

Q

Major waveform 24Vin 5Vout at 2A 583kHz operation:

12Vout at 2A similar waveform, but longer on time

13-Məy-14

17:40:08





5V 2A output ripple at full load at output cap – 24Vin: TPS54335DDA 13-May-14



Bode plots: 24Vin 583kHz actual switching frequency TPS54335DDA 5V setting load 1 A

Josh Mandelcorn



Bode plots for 12V setting: TPS54335DDA Load 1 A

Load 2 A



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